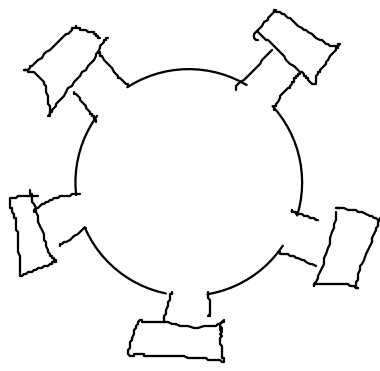


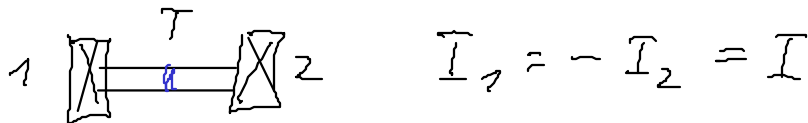
and so



$$\frac{h}{2e} I_\alpha = [N_\alpha - R_\alpha] \mu_\alpha - \sum_{\beta \neq \alpha} T_{\alpha\beta} \mu_\beta$$

Beispiele

1) 2 Kontakt - System



$$I_1 = -I_2 = I$$

$$T_{12} = T_{21} = T; \quad R_1 = R_2 = R = N - T$$

(wählt man N zu groß,
wird mehr Reflektivität)

Zahl der Kanäle,
(beliebig)

$$\frac{h}{2e} I = [N - R] \mu_1 - T \mu_2$$

$$-\frac{h}{2e} I = [N - R] \mu_2 - T \mu_1$$

Differenz

$$2 \frac{h}{2e} I = [N - R] (\mu_1 - \mu_2) + T (\mu_1 - \mu_2)$$

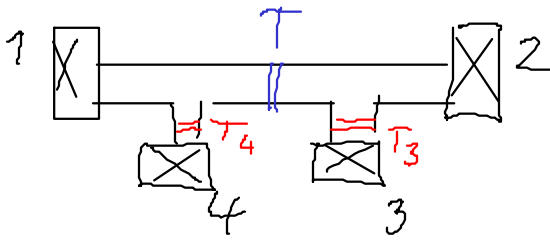
$$= (N - R + T) (\mu_1 - \mu_2) = 2T (\mu_1 - \mu_2)$$

$$\Rightarrow I = \frac{2e}{h} (\mu_1 - \mu_2) = G_{2P} \frac{\mu_1 - \mu_2}{e}$$

Summe

$$0 = (N - R) (\mu_1 + \mu_2) - T (\mu_1 + \mu_2) = 0 \checkmark$$

2) 4-Kontakt-System mit 1 Kanal



T_3 und T_4 sollen eine schwache Kopplung der Spannung-Messkontakte bringen

zu Vereinfachung $T_3 = T_4 = \sigma \ll 1 \Rightarrow T_{31}, T_{41} \ll 1$

$$(1) \quad \frac{h}{2e} I = (1 - R_1) \mu_1 - T_{12} \mu_2 - T_{13} \mu_3 - T_{14} \mu_4$$

$$(2) \quad -\frac{h}{2e} I = (1 - R_2) \mu_2 - T_{21} \mu_1 - T_{23} \mu_3 - T_{24} \mu_4$$

$$(3) \quad 0 = (1 - R_3) \mu_3 - T_{31} \mu_1 - T_{32} \mu_2 - \cancel{T_{34} \mu_4}$$

$$(4) \quad 0 = (1 - R_4) \mu_4 - T_{41} \mu_1 - T_{42} \mu_2 - \cancel{T_{43} \mu_3}$$

Abstraktion:

$$T_{12} = T_{21} = T + O(\sigma)$$

$$T_{13} = T\sigma = T_{31} = T_{24} = T_{42}$$

$$T_{14} = \sigma + R\sigma = T_{41} = T_{23} = T_{32}$$

$$R = 1 - T$$

vernachlässige $T_{34} = \sigma^2 T = T_{43} \ll 1$

(3) - (4)

$$0 = (1 - R_3)(\mu_3 - \mu_4) - T_{31}(\mu_1 - \mu_2) - T_{32}(\mu_2 - \mu_1)$$

$$0 = (T_{13} + T_{23} + \cancel{T_{43}})(\mu_3 - \mu_4) - (T_{32} - T_{31})(\mu_2 - \mu_1)$$

$$\Rightarrow \mu_3 - \mu_4 = \frac{T_{32} - T_{31}}{T_{32} + T_{31}} (\mu_2 - \mu_1) = \frac{\sigma(1+R) - \sigma T}{\sigma(1+R) + \sigma T} (\mu_2 - \mu_1)$$

$$= \frac{2R}{2} (\mu_2 - \mu_1)$$

$$\Rightarrow \mu_3 - \mu_4 = R(\mu_2 - \mu_1)$$

(1) - (2)

$$\frac{2h}{2e} I = (1-R)(\mu_1 - \mu_2) - T_{22}(\mu_2 - \mu_1) + \sigma(\sigma)$$

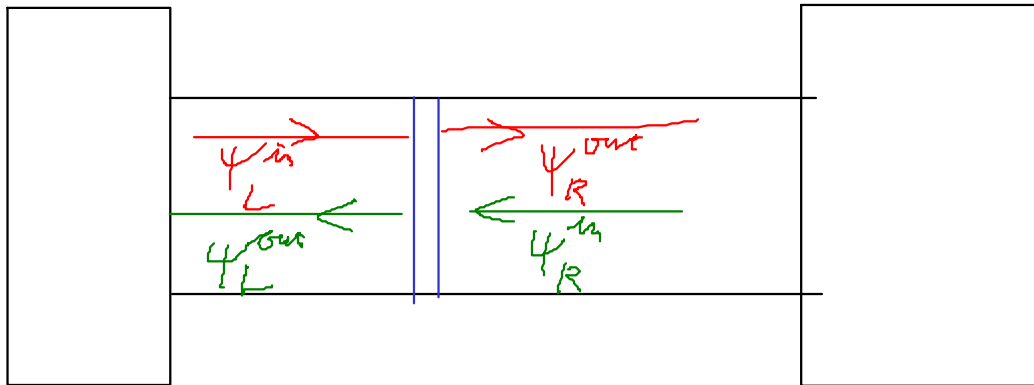
$$= (1-R+T)(\mu_1 - \mu_2)$$

$$= 2T(\mu_1 - \mu_2)$$

$$\Rightarrow G_{2p} = \frac{eI}{\mu_1 - \mu_2} = \frac{2e^2}{h} T$$

$$\text{und } G_{4p} = \frac{eI}{\mu_4 - \mu_3} = \frac{eI}{R(\mu_1 - \mu_2)} = \frac{2e^2}{h} \frac{T}{R}$$

2.8 S-Matrix für Streuung



$$\psi_L^{\text{in}}(x, y) = \sum_{n=1}^M a_n^L \chi_n^L(y) e^{ik_n x}$$

$$\psi_L^{\text{out}}(x, y) = \sum_{n=1}^M b_n^L \chi_n^L(y) e^{-ik_n x}$$

$$\psi_R^{\text{in}}(x, y) = \sum_{m=1}^{NR} a_m^R \chi_m^R(y) e^{ik_m x}$$

$$\psi_R^{\text{out}}(x, y) = \sum_{m=1}^{NR} b_m^R \chi_m^R(y) e^{-ik_m x}$$

$$S\text{-Matrix} \begin{pmatrix} b_1^L \\ b_2^L \\ \vdots \\ b_N^L \\ b_1^R \\ b_2^R \\ \vdots \\ b_N^R \end{pmatrix} = \begin{pmatrix} r_{11} & r_{12} & \dots & r_{1N_L} & t_{11}^i & t_{1N_R}^i \\ \vdots & \vdots & & \vdots & \vdots & \vdots \\ r_{N_L 1} & \dots & r_{N_L N_L} & t_{N_L 1}^i & t_{N_L N_R}^i \\ \hline t_{11}^r & & t_{1N_L}^r & r_{11}^i & r_{N_R 1}^i \\ \vdots & & \vdots & \vdots & \vdots \\ t_{N_R 1}^r & & t_{N_R N_L}^r & r_{N_R 1}^i & r_{N_R N_R}^i \end{pmatrix} \begin{pmatrix} a_1^L \\ a_2^L \\ \vdots \\ a_N^L \\ a_1^R \\ \vdots \\ a_N^R \end{pmatrix}$$

$a_1^L \Rightarrow b_1^L$ Kanal 1 reflektiv nach Kanal 1 $\Rightarrow r_{11}$
 $a_1^L \Rightarrow b_1^R$ Kanal 1 transmittiv auf Kanal 1 $\Rightarrow t_{11}^r$

S ist quadrat. $(N_L + N_R)^2$ Matrix

$$b = S \cdot a \quad \text{oder (symbolisch)} \quad \psi^{\text{out}} = S \psi^{\text{in}}$$

$(N_L + N_R)$ dim. Vektoren

Die S -Matrix kann auf mehrere Kontakte verallgemeinert werden $S \leftrightarrow t_{d\beta, mm} ; r_{d\alpha, mm}$

Eigenschaften

a) Beh S ist unitar $S S^\dagger = S^\dagger S = 1$

$$\Rightarrow \langle \psi^{\text{in}} | \psi^{\text{in}} \rangle =$$

$$\int dx dy \sum_{m=1}^{N_L+N_R} \sum_{m'=1}^{N_L+N_R} a_m^* a_{m'} x_m^*(y) x_{m'}(y) e^{\pm i k_n x} e^{\pm i k_{m'} x}$$

$$= L \sum_m |a_m|^2$$

Orthogonalität nutzen

$$\begin{aligned}
 \langle \psi^{\text{out}} | \psi^{\text{out}} \rangle &= L \sum_m |b_m|^2 \quad (\text{analog}) \\
 &= L \sum_{m, m'} S_{mm'}^* a_{m'}^* S_{mm} a_m \\
 &= L \sum_{m, m'} (S^\dagger S)_{m'm} a_{m'}^* a_m = L \sum_m |a_m|^2 \\
 &= \langle \psi^{\text{in}} | \psi^{\text{in}} \rangle
 \end{aligned}$$

das Beweist nicht dass S unitär sein muss

auch $\langle \psi^{\text{out}} | \psi^{\text{out}} \rangle = \langle \psi^{\text{in}} | \psi^{\text{in}} \rangle$
 warum? kein phys. Gesetz

jetzt: Beweis dass S unitär folgt aus Stromerhaltung

$$\begin{aligned}
 I_L^{\text{in}} &= \text{Re} \frac{e}{m} \int dy \psi_L^{\text{in}*} (-i\hbar \nabla_x) \psi_L^{\text{in}} \\
 &= \frac{e\hbar}{m} \sum_{n=1}^{N_L} |a_n|^2 k_n \quad (?)
 \end{aligned}$$

$$I_L = I_L^{\text{in}} - I_L^{\text{out}} = I_R = I_R^{\text{out}} - I_R^{\text{in}} \quad (\text{rechts} = \text{links})$$

$$\Rightarrow I_L^{\text{in}} + I_R^{\text{in}} = I_L^{\text{out}} + I_R^{\text{out}} \quad (\text{in} = \text{out})$$

$$\Rightarrow \sum_{n=1}^{N_L+N_A} |a_n|^2 k_n = \sum_{n=1}^{N_L+N_R} |b_n|^2 k_n$$

$$\frac{m}{e\hbar} I^{\text{out}} = \sum_{m=1} |b_m|^2 k_m = \sum_m \sum_{n,n'} S_{mm}^* a_n S_{mm'} a_{n'} k_m$$

$$= \sum_{n,n'} \sum_m S_{nm}^+ S_{mm'} k_m a_n^* a_{n'}$$

führe neue Matrix ein

$$\begin{aligned}
 \tilde{S}_{mn} &= S_{mn} \sqrt{\frac{k_m}{k_n}} \quad \Leftrightarrow \quad S_{mn} = \sqrt{\frac{k_m}{k_n}} \tilde{S}_{mn} \\
 \Rightarrow \tilde{S}_{mn}^+ &= \tilde{S}_{nm}^* = S_{nm}^* \sqrt{\frac{k_m}{k_n}} = S_{mn}^+ \sqrt{\frac{k_m}{k_n}}
 \end{aligned}$$

$$S_{mm'}^+ = \tilde{S}_{mm'}^+ \sqrt{\frac{k_m}{k_m}}$$

$$= \sum_{m, m'} \sum_m \tilde{S}_{mm'}^+ \sqrt{\frac{k_m}{k_m}} \tilde{S}_{mm'} \sqrt{\frac{k_{m'}}{k_m}} k_m a_m^* a_{m'}$$

$$= \sum_{m, m'} \left(\sum_m \tilde{S}_{mm}^+ \tilde{S}_{mm'} \right) \sqrt{k_m k_{m'}} a_m^* a_{m'}$$

wenn $\tilde{S}^+ \tilde{S} = \mathbb{1}$ also \tilde{S} unitär

$$= \sum_m |a_m|^2 k_m \quad \checkmark \quad \text{Stromerhaltung}$$

folgt aus \tilde{S} unitär auch S unitär?

$$\sum_m S_{mm}^+ S_{mm'} = \sum_m \tilde{S}_{mm}^+ \sqrt{\frac{k_m}{k_m}} \tilde{S}_{mm'} \sqrt{\frac{k_{m'}}{k_m}}$$

$$\sqrt{\frac{k_m}{k_m}} \sqrt{\frac{k_{m'}}{k_m}} \Rightarrow \mathbb{1}$$

b) Für Zeitumkehrinvariante Probleme

$$\Rightarrow S = S^T \quad \Rightarrow t_{mm} = t_{mm}$$

$$t_{\alpha\beta mm} = t_{\beta\alpha mm}$$

$$\Rightarrow G_{\alpha\beta} = G_{\beta\alpha}$$

mit Magnetfeld nicht Zeitumkehrinvariant

$$S(\vec{B}) = S^T(-\vec{B}) \quad \rightarrow t_{\alpha\beta mm}(\vec{B}) = t_{\beta\alpha mm}(-\vec{B})$$

$$\rightarrow G_{\alpha\beta}(\vec{B}) = G_{\beta\alpha}(-\vec{B})$$